

Form B

99

Q1)

1- Non Dispersion Shifted fiber

① optimized at 1300 nm

2- Dispersion shifted fiber

3- Dispersion flattened fiber

4- Dispersion compensating fiber

5- large effective core area fiber

Dispersion shifted fiber has zero at 1550 nm

Non Dispersion shifted fiber has maximum attenuation

Q2) $L = 50 \text{ km}$

$P_{in} = 1 \text{ mW}$

$\alpha = 0.5 \text{ dB/km}$

① $P_{out} = P_{in} \text{ dBm} - \text{loss}$

$= -25 \text{ dB}$

$P_{in} \text{ dBm} = 10 \log \left(\frac{1 \times 10^{-3}}{10^{-6}} \right) = 30 \text{ dBm}$

$P_{out} \text{ dBm} = 30 - 25 = 5 \text{ dBm}$

~~10 dB~~

$$10 \log(P_{out} \text{ mW}) = 5$$

$$P_{out} = 3.1 \text{ mW}$$

Q3)

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- 1- ~~TE_{0m} mode~~
- 2- ~~TM_{0m} mode~~
- 3- ~~HE_{11m} mode~~ $v > 1$
- 4- ~~EH_{11m} mode~~ $v > 1$

HE₁₁ is the dominant mode

EH_{11m} mean

$E_2 > H_2$
in Amplitude

Electric wave \rightarrow

Amplitude
magnetic wave

Q4)

$$n_1 = 1.46 \quad \Delta = 0.25\%$$

wanted maximum q

$$V = 2.405$$

$$\lambda = 1300 \text{ nm}$$

$$V = \frac{2\pi a}{\lambda} \text{ NA}$$

$$\text{NA} = n_1 \sqrt{2\Delta} = 1.46 \times \sqrt{2 \times 0.25\%} = 0.103$$

$$2.405 = \frac{2\pi a \times 0.103}{1300 \times 10^{-9}} \Rightarrow a = \frac{2.405 \times 1300 \times 10^{-9}}{2\pi \times 0.103}$$

$$a = 4.88 \text{ mm}$$

$$V = \frac{2\pi a}{\lambda} \text{ NA}$$

for $\lambda = 1550$

$$V = 2.0171 < 2.405 \quad \text{yes it can use}$$

for $\lambda = 850 \text{ nm}$

$$V = 3.67 > 2.405$$

it can't support this wave
at $\lambda = 850 \text{ nm}$

wave

Q5) 1- Single mode fiber
advantage 1- highest bandwidth

Type
single mode fiber
step index

Advantage
highest bandwidth

disadvantage
highest cost

multi-mode step index

lowest splicing loss
~~highest~~

the lowest bandwidth

multi-mode graded index

Highest power
avalanche

low in bandwidth
with respect
to single mode

$$n_1 = 1.42$$

$$n_2 = 1.46$$

$$\lambda = 1300 \text{ nm}$$

critical θ_c

$$NA, \theta_{\text{max}}$$

$$\Delta, M$$

$$\theta_c = \sin^{-1}\left(\frac{n_2}{n_1}\right) = 80.57^\circ$$

$$2- NA = \sqrt{n_1^2 - n_2^2} = 0.2425$$

$$3- \sin \theta_{\text{max}} = \sqrt{n_1^2 - n_2^2}$$

$$\theta_{\text{max}} = \sin^{-1}(NA) = 14^\circ$$

$$4- \Delta = \frac{n_1 - n_2}{n_1} = 0.0135$$

$$5- M = \frac{V^2}{2} = \frac{(2.59 NA)^2}{2}$$

$$V = \frac{2.59 NA}{\lambda} = \frac{2.59 \times 2.5 \times 10^{-6} \times 0.2425}{1300 \times 10^{-9}}$$

$$= 29.3$$

$$M = 429.3 \text{ modes}$$

Form B

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Q7)

- 1 - Chromatic dispersion
- 2 - modal dispersion
- 3 - polarization dispersion

largest one is the modal dispersion

the lowest or smallest one is the polarization dispersion

Q8)

preform

$$D = 10 \text{ mm}$$

$$L = 100 \text{ cm}$$

$$\text{fiber diameter } d = 125 \text{ } \mu\text{m}$$

From the conservation of mass

Volume of preform = Volume of fiber

$$\pi \left(\frac{D}{2}\right)^2 L = \pi \left(\frac{d}{2}\right)^2 L$$

$$\left(5 \times 10^3\right)^2 \times 100 \times 10^{-2} = \left(\frac{125 \times 10^{-6}}{2}\right)^2 \times L$$

$$L = 6400 \text{ m}$$

9.)

1- it's able to make thin, flexible long optical wire

2- it's transparent for a particular ~~fiber~~ wavelength

the three are

1- outside vapor deposition

2- vapor axial deposition

3- modified chemical vapor deposition

Q 10) $L = 50 \text{ km}$ single mode

$n_1 = 1.48$ $\Delta = 0.005$

$D_{mat} = 5 \text{ ps / (km nm)}$

$$\left[\frac{d^2 v_b}{dv^2} \right] = 0.5$$

$$\Delta \lambda = 2 \text{ nm}$$

$$\lambda = 1550 \text{ nm}$$

wanted the chromatic dispersion

$$\sigma_{mat} = D_{mat} L \sigma_1$$

$$= 5 \times 50 \times 2 = 500 \text{ ps}$$

$$\sigma_{wg} = D_{wg} L \sigma_1$$

$$D_{wg} = - \frac{n_2 \Delta}{\lambda c} \left[v d^2 \frac{v}{dv^2} \right]$$

$$\Delta = \frac{n_1 - n_2}{n_1} \Rightarrow n_2 = 1.4726$$

$$D_{wg} = - \frac{1.4726 \times 0.005}{1550 \text{ (nm)} \times 3 \times 10^5 \text{ (km)}} \left[0.5 \right]$$

$$D_{wg} = -7.917 \text{ ps/(nm.km)}$$

$$\sigma_{wg} = \frac{-15.83 \times 50 \times 2}{2} = -791.7 \text{ ps}$$

$$\sigma_{Chro} = \sigma_{wg} + \sigma_{mat} =$$

$$= -791.7 \text{ ps} + 500 \text{ ps} = -291.7 \text{ ps}$$

$\frac{1}{\sigma_{Chro}}$

$$B_T = \frac{1}{\sigma_{Chro}} = \frac{1}{-291.7 \text{ ps}} = -3.46 \text{ GHz}$$

$$\text{Band width product} = 50 * 3.43 \text{ GHz}$$

$$= \cancel{46163} \text{ MHz.km}$$

$$= \cancel{46163} \text{ MHz.km}$$

$$= 171.41 \text{ GHz.km}$$